Frequency dependent correlations - simple tool for time series analysis

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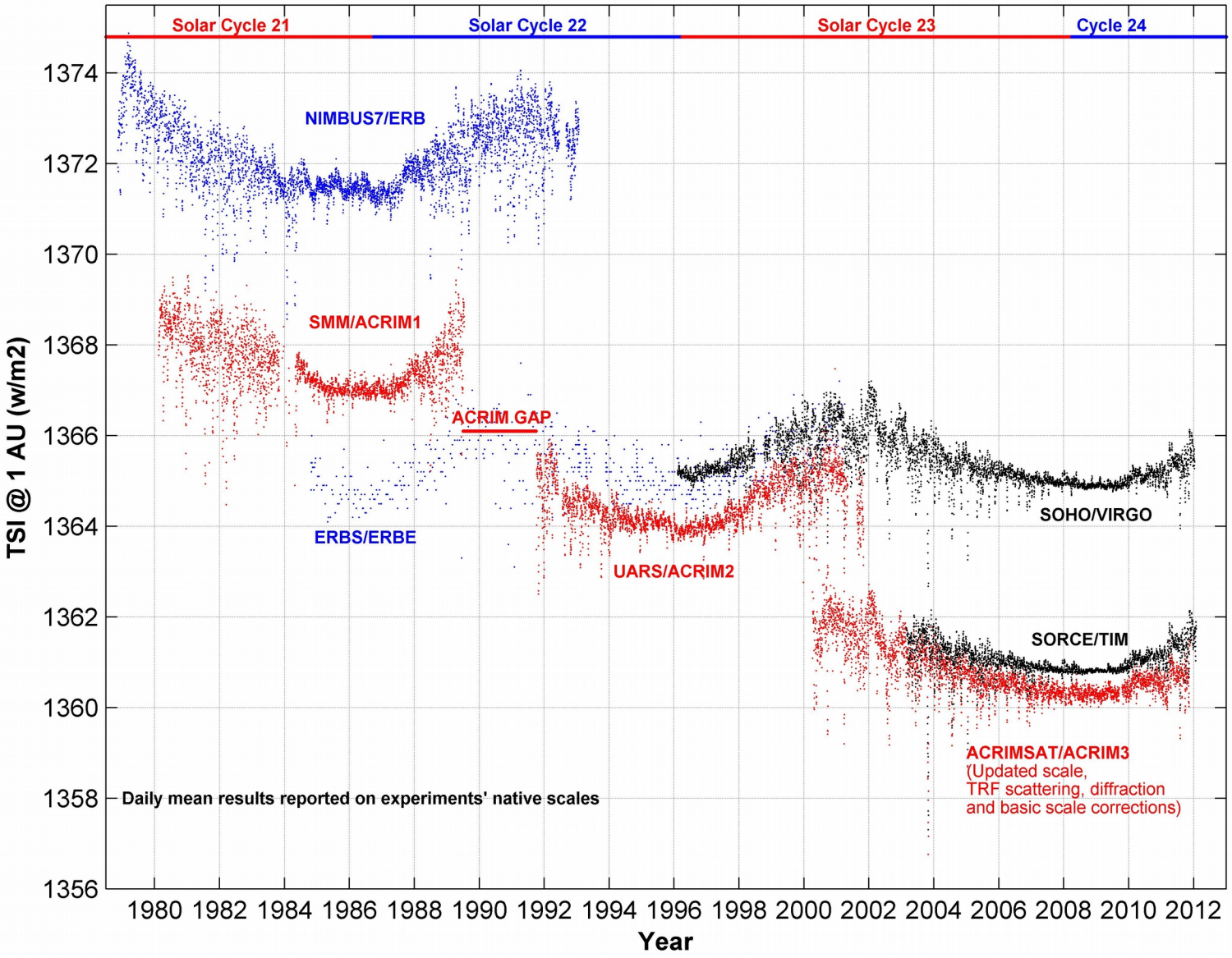
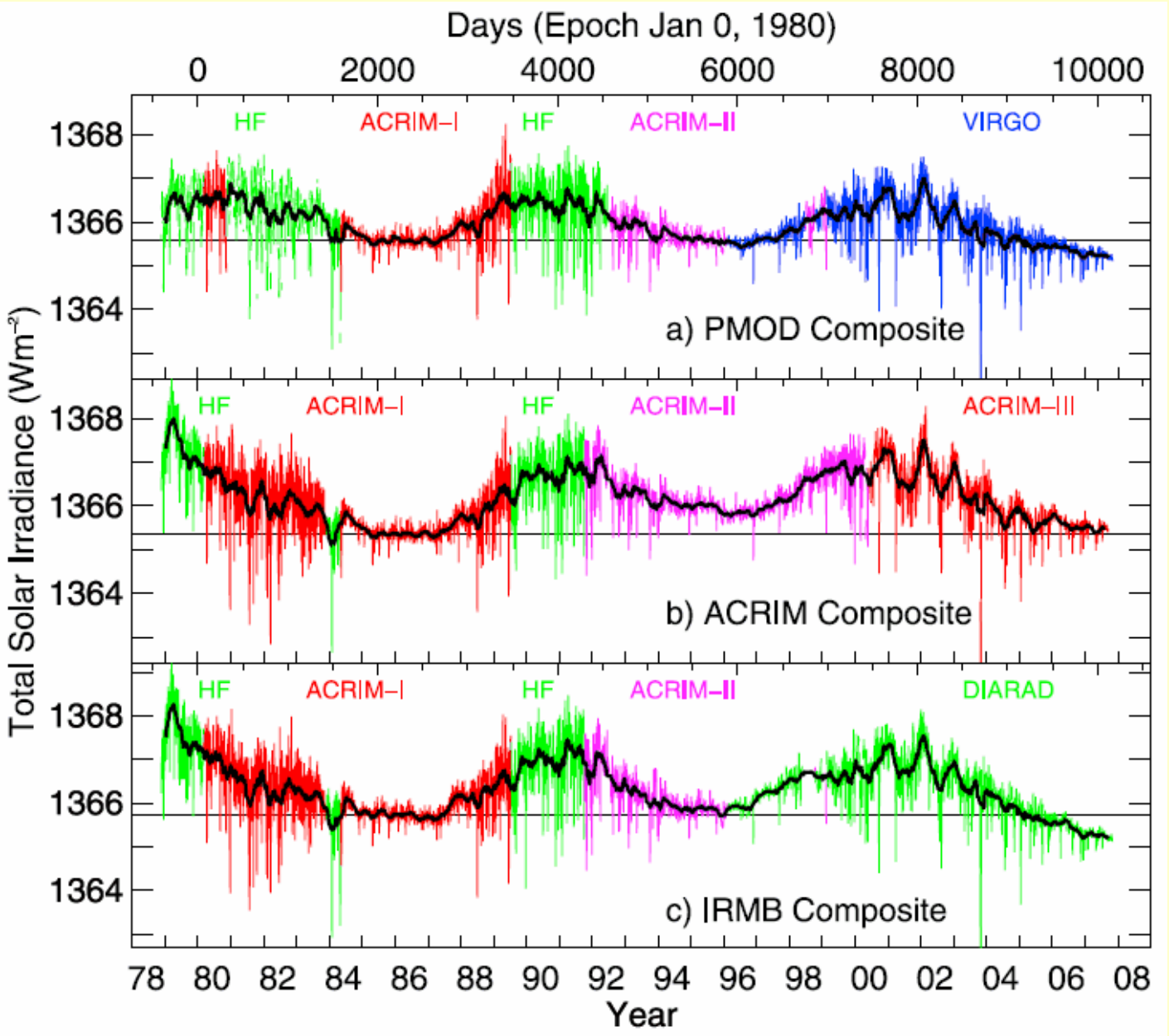
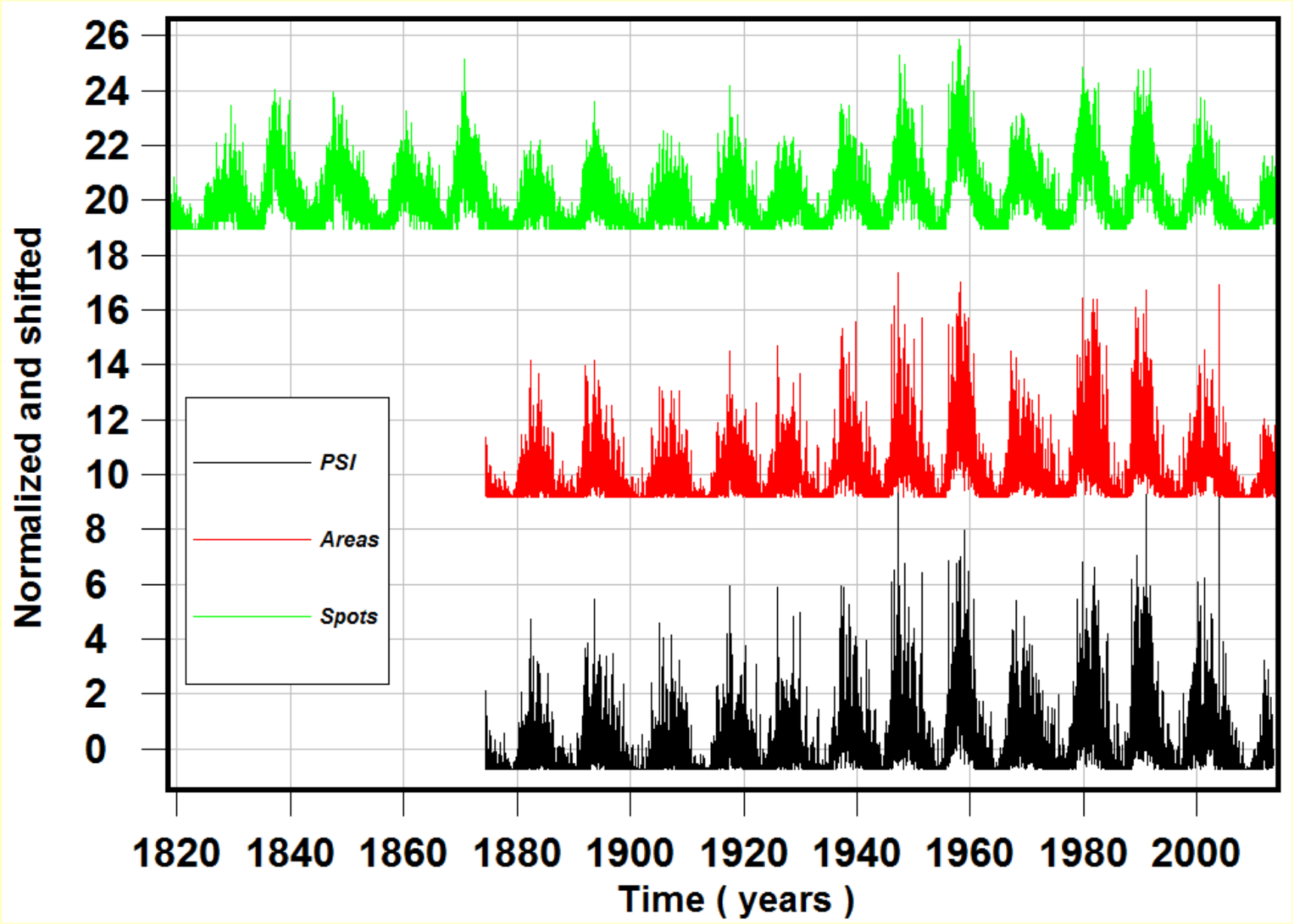
TOTAL SOLAR IRRADIANCE MONITORING RESULTS: 1978 to Present



RC Willson, earth_obs_fig1 03/01/2012



Three targets – TSI Composites


Normalized and shifted
26
24
22
20
18
16
14
12
10
8
6
4
2
0
PSI
Areas
Spots
1820
1840
1860
1880
1900
1920
1940
1960
1980
2000
Time (years)

Proxies

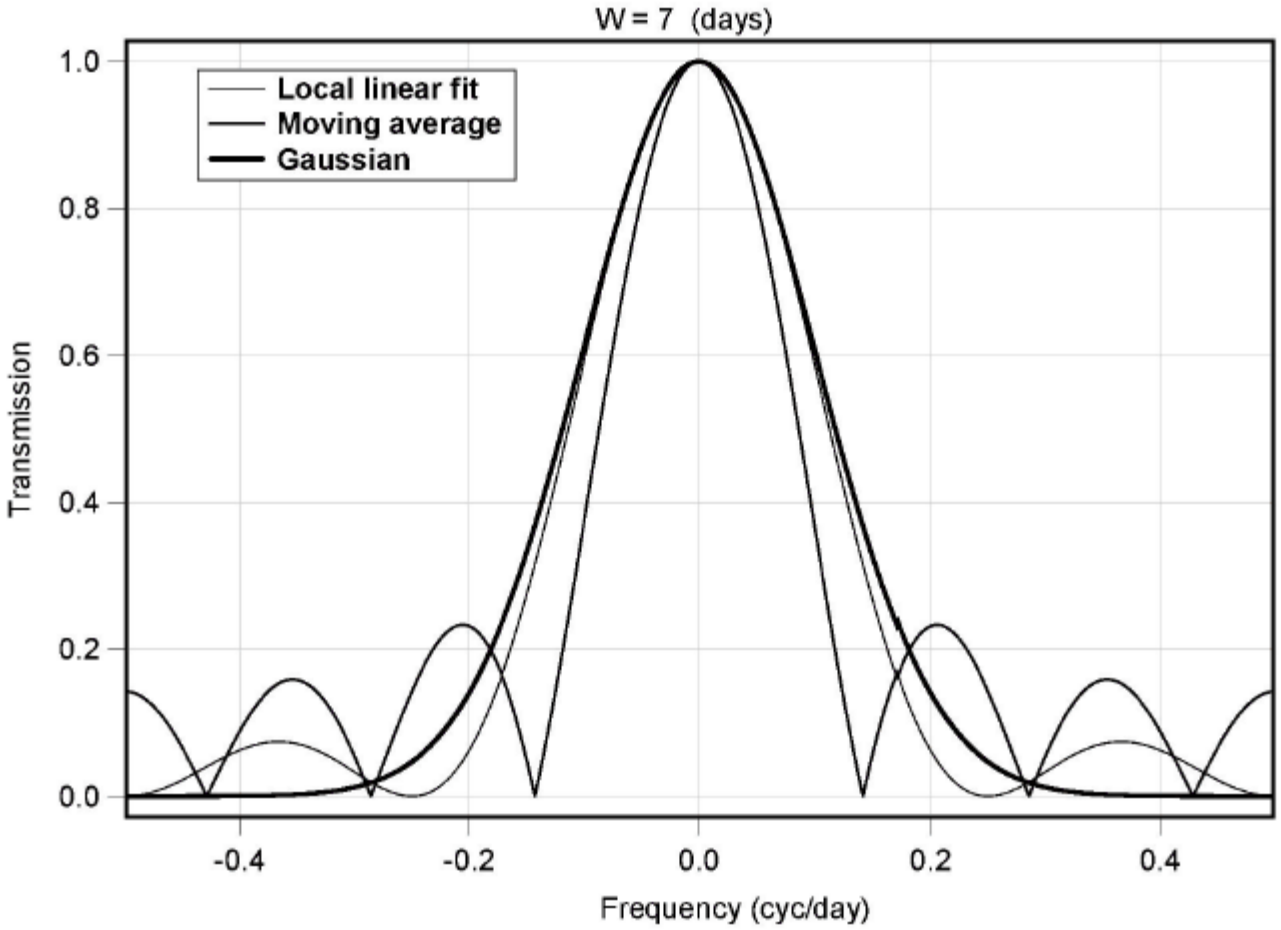


Fig. 1. Three different transmission curves for the specific width of the time domain filter.

$$T(\nu) = \exp^{-(\nu W)^2}$$

Transmission curve for Gaussian filter

Data -> FFT -> Multiple by TC -> FFT^{-1} =Smoothed data

LF part = smoothed data
HF part = data – smoothed data

To compare different daily data sets we:

A. Cut off parts for which both data exist.

B. Compute R_c= $$\frac{\sum_{i=1}^{n}(x_i-\bar{x})(y_i-\bar{y})}{\sqrt{\sum_{i=1}^{n}(x_i-\bar{x})^2}\sqrt{\sum_{i=1}^{n}(y_i-\bar{y})^2}}$$

	PMOD	RMIB	ACRIM	SATIRE-S
Original				
PMOD	1.0000	**0.9322**	0.8553	0.8969
RMIB	**0.9322**	1.0000	0.9167	0.8586
ACRIM	0.8553	0.9167	1.0000	*0.8105*
SATIRE-S	0.8969	0.8586	*0.8105*	1.0000
LF				
PMOD	1.0000	0.9191	0.8422	**0.9446**
RMIB	0.9191	1.0000	0.9022	0.8404
ACRIM	0.8422	0.9022	1.0000	*0.7962*
SATIRE-S	**0.9446**	0.8404	*0.7962*	1.0000
HF				
PMOD	1.0000	0.9391	0.8939	0.8583
RMIB	0.9391	1.0000	**0.9424**	0.8777
ACRIM	0.8939	**0.9424**	1.0000	*0.8266*
SATIRE-S	0.8583	0.8777	*0.8266*	1.0000

Table 2. Correlation matrices for input target sets.

	PSI	SA	SN	RADIO	MGII	LYMAN
Original						
PSI	1.0000	0.9424	0.8521	0.8722	0.7726	*0.7709*
SA	0.9424	1.0000	0.8786	0.9041	0.8001	0.8116
SN	0.8521	0.8786	1.0000	0.9466	0.9237	0.9116
RADIO	0.8722	0.9041	0.9466	1.0000	0.9616	0.9552
MGII	0.7726	0.8001	0.9237	0.9616	1.0000	**0.9735**
LYMAN	*0.7709*	0.8116	0.9116	0.9552	**0.9735**	1.0000
LF						
PSI	1.0000	**0.9978**	0.9890	0.9943	0.9885	0.9896
SA	**0.9978**	1.0000	0.9880	0.9890	*0.9822*	0.9822
SN	0.9890	0.9880	1.0000	0.9915	0.9858	0.9841
RADIO	0.9943	0.9890	0.9915	1.0000	0.9968	0.9930
MGII	0.9885	*0.9822*	0.9858	0.9968	1.0000	0.9900
LYMAN	0.9896	0.9822	0.9841	0.9930	0.9900	1.0000
HF						
PSI	1.0000	**0.8939**	0.7410	0.8172	0.5715	0.5852
SA	**0.8939**	1.0000	0.7452	0.8315	*0.5527*	0.5909
SN	0.7410	0.7452	1.0000	0.8020	0.7054	0.6663
RADIO	0.8172	0.8315	0.8020	1.0000	0.8047	0.8014
MGII	0.5715	*0.5527*	0.7054	0.8047	1.0000	0.8725
LYMAN	0.5852	0.5909	0.6663	0.8014	0.8725	1.0000

Table 1. Correlation matrices for input proxy data sets.

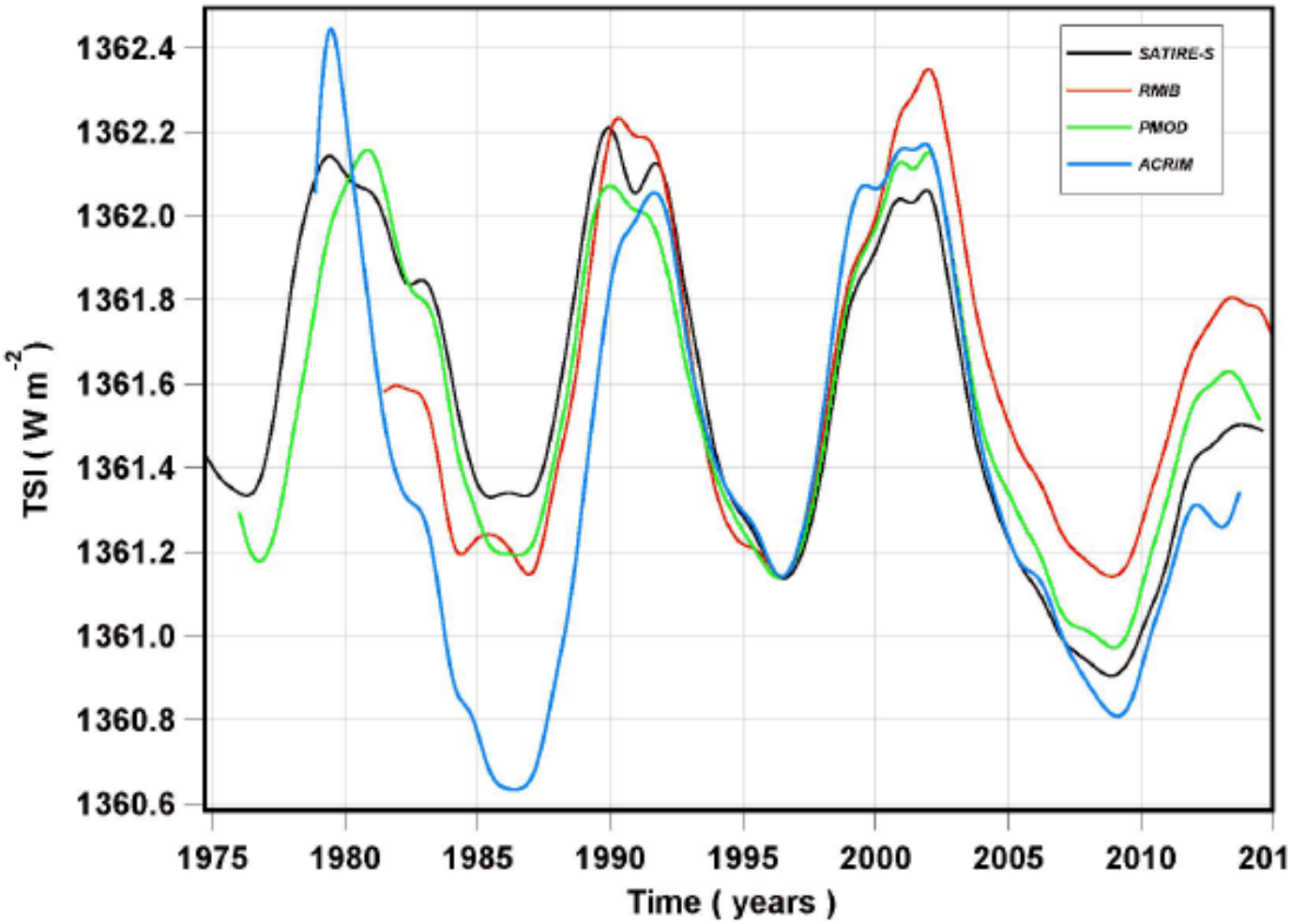
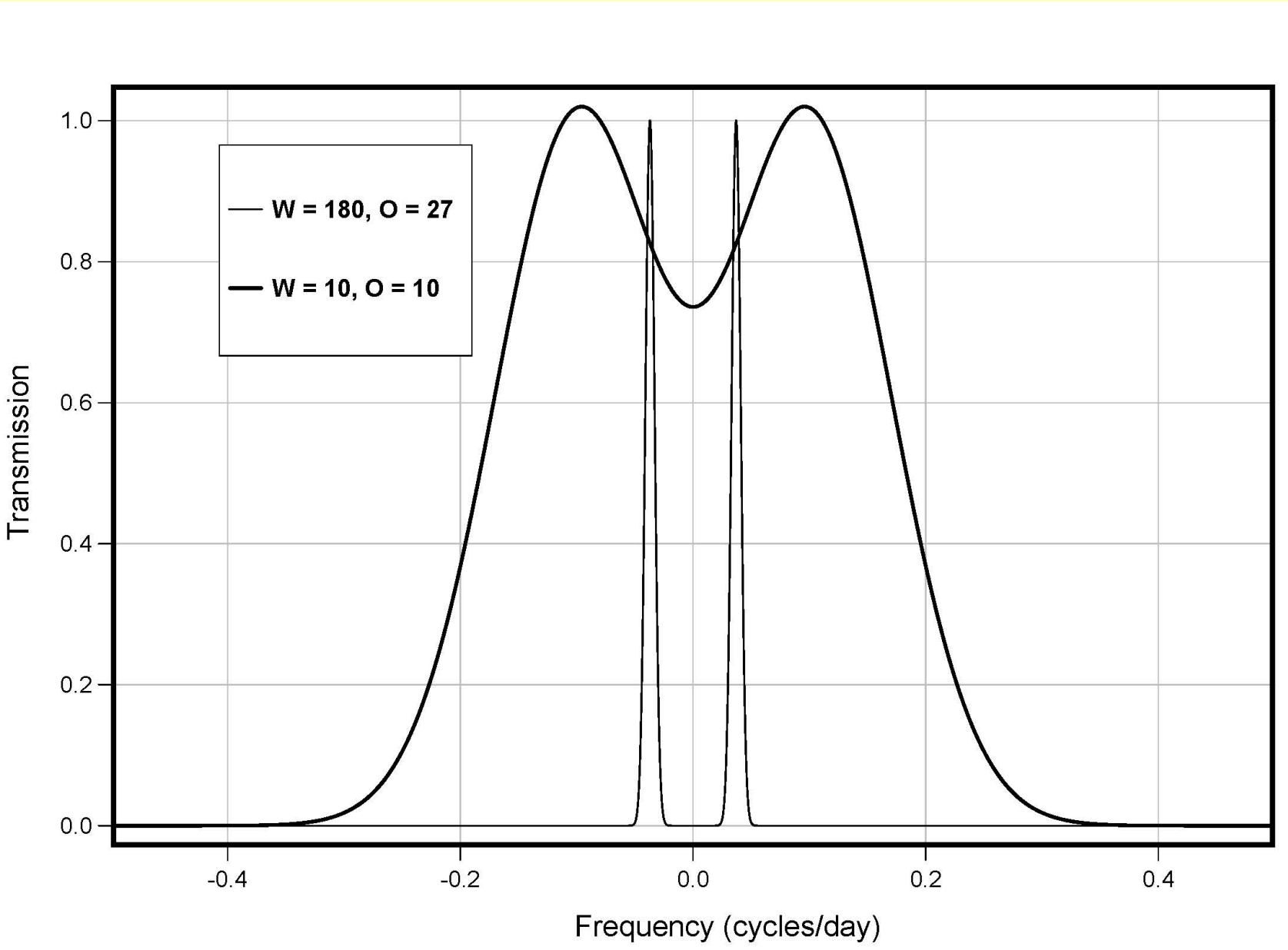
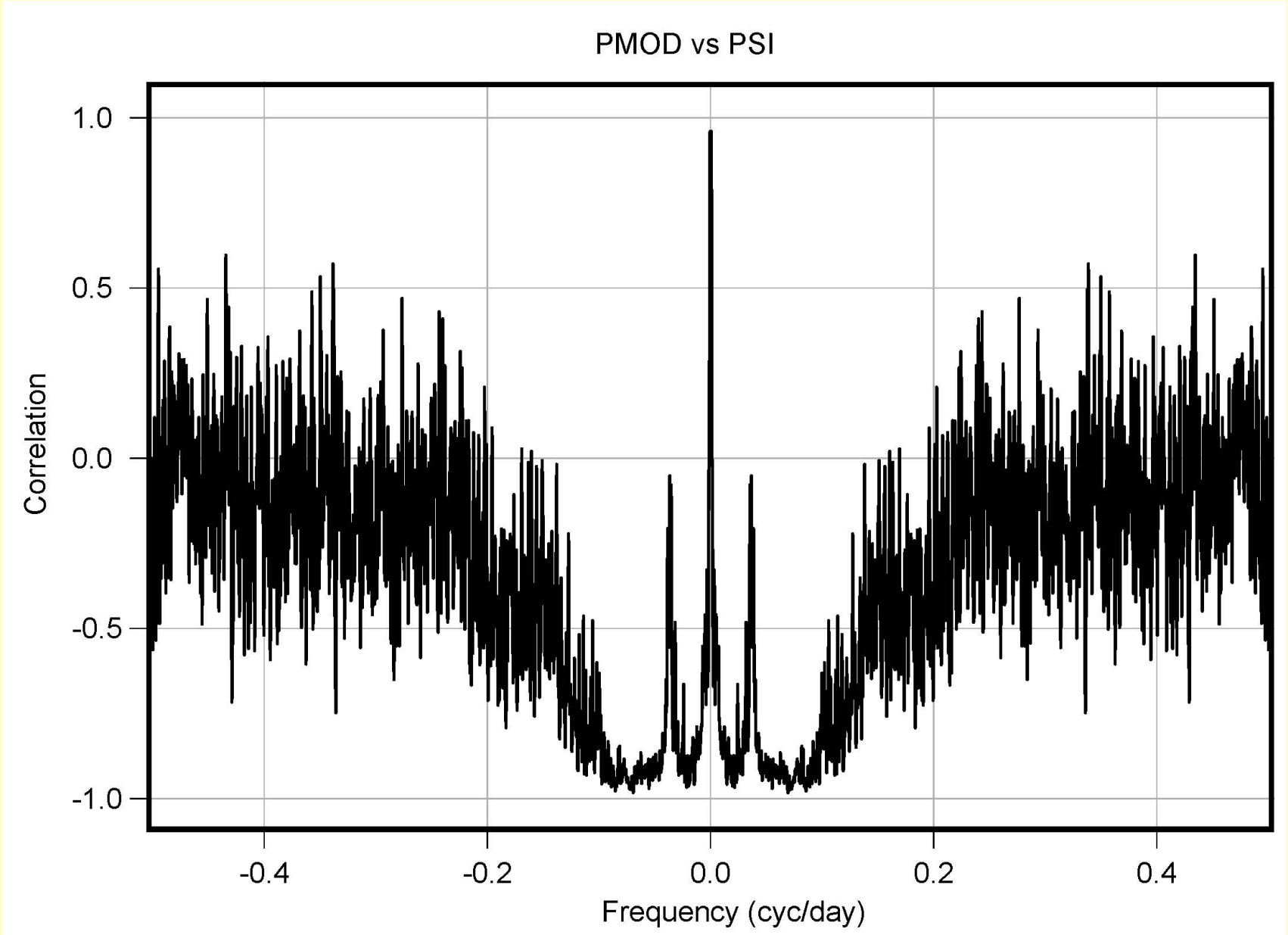
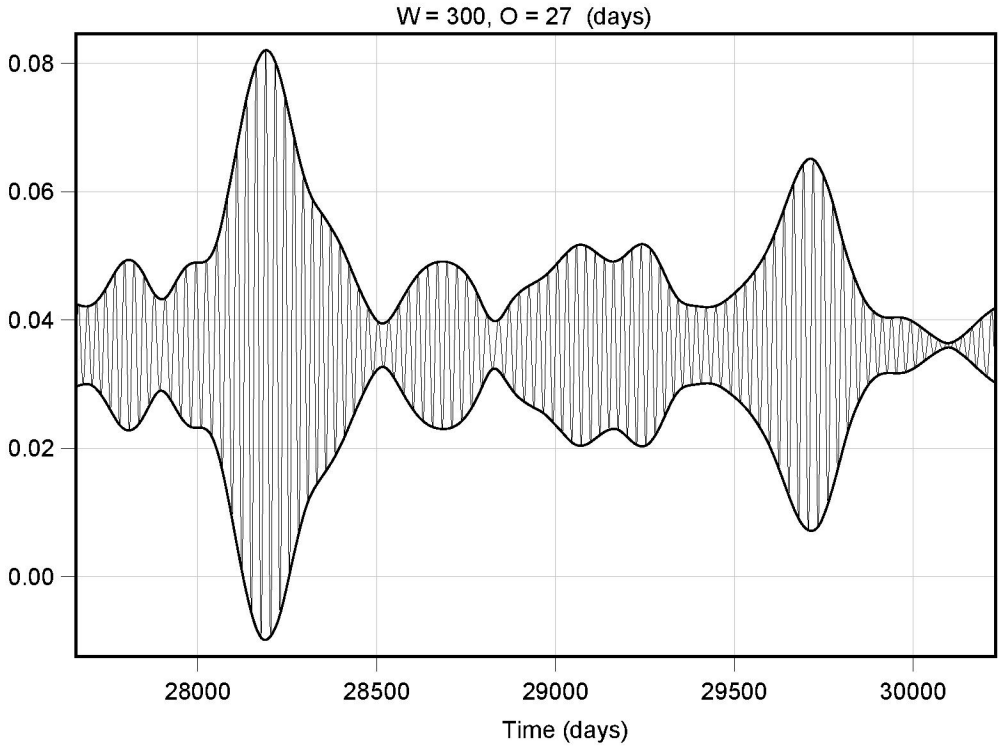


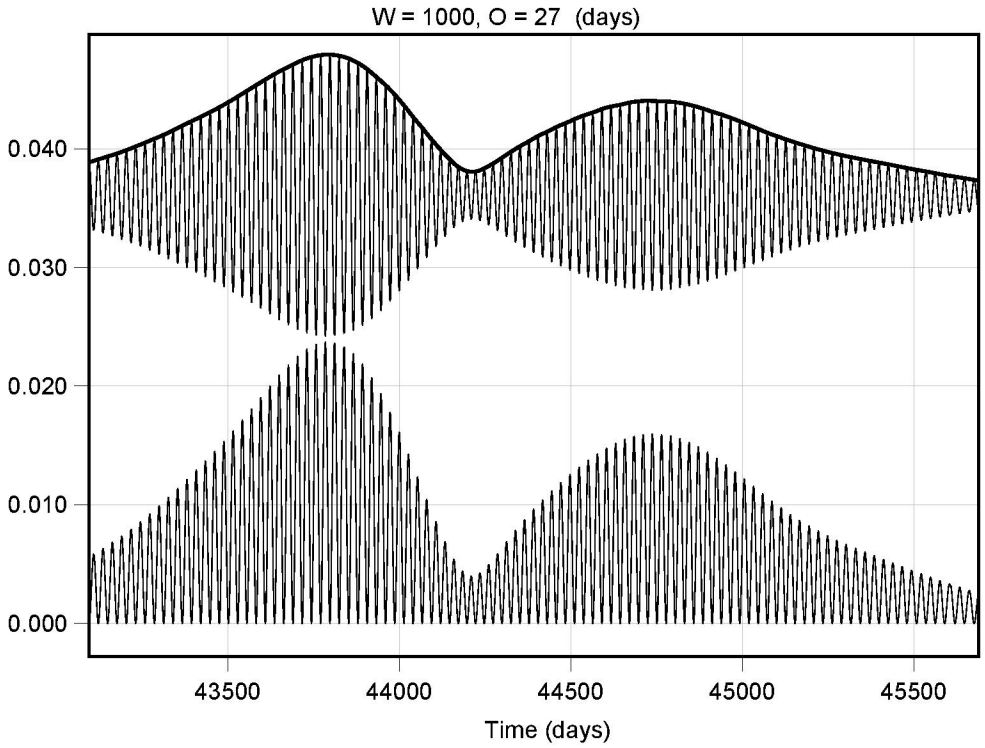
Fig. 6. The major controversy. To recover TSI for the past dates we need current estimates for calibration. But which one to choose? LF parts ($W = 750$ days) of four target TSI composites. The input curves are shifted to common level at 1996.465.


W = 180, O = 27
W = 10, O = 10
Transmission
1.0
0.8
0.6
0.4
0.2
0.0
-0.4
-0.2
0.0
0.2
0.4
Frequency (cycles/day)



W = 2000 days, varying offsets


W = 300, O = 27 (days)
0.08
0.06
0.04
0.02
0.00
28000
28500
29000
29500
30000
Time (days)


W = 1000, O = 27 (days)
0.040
0.030
0.020
0.010
0.000
43500
44000
44500
45000
45500
Time (days)

$$SS = \sum_{i=1}^{N} \left(y(t_i) - \sum_{l=0}^{L} a_l E_l(\ldots)[t_i] \right)^2$$

- Start model building from including into it constant level and the input curve as components.
- In each additional step try all the variants from the full library of filtered or otherwise processed components to be as possible next components.
- Evaluate prospective candidates by correlating obtained model with actually observed signal.
- Finally, use the obtained model to hindcast unobserved irradiance values.

Coefficent	Predictor	Value
a_0	1.0	1365.551
a_1	$E(0,0)$	-8.030
a_2	$E(766.229, 0.0)$	19.049
R_c	0.8597	

Table 4. Summary of least squares fit results with one smoothed component.

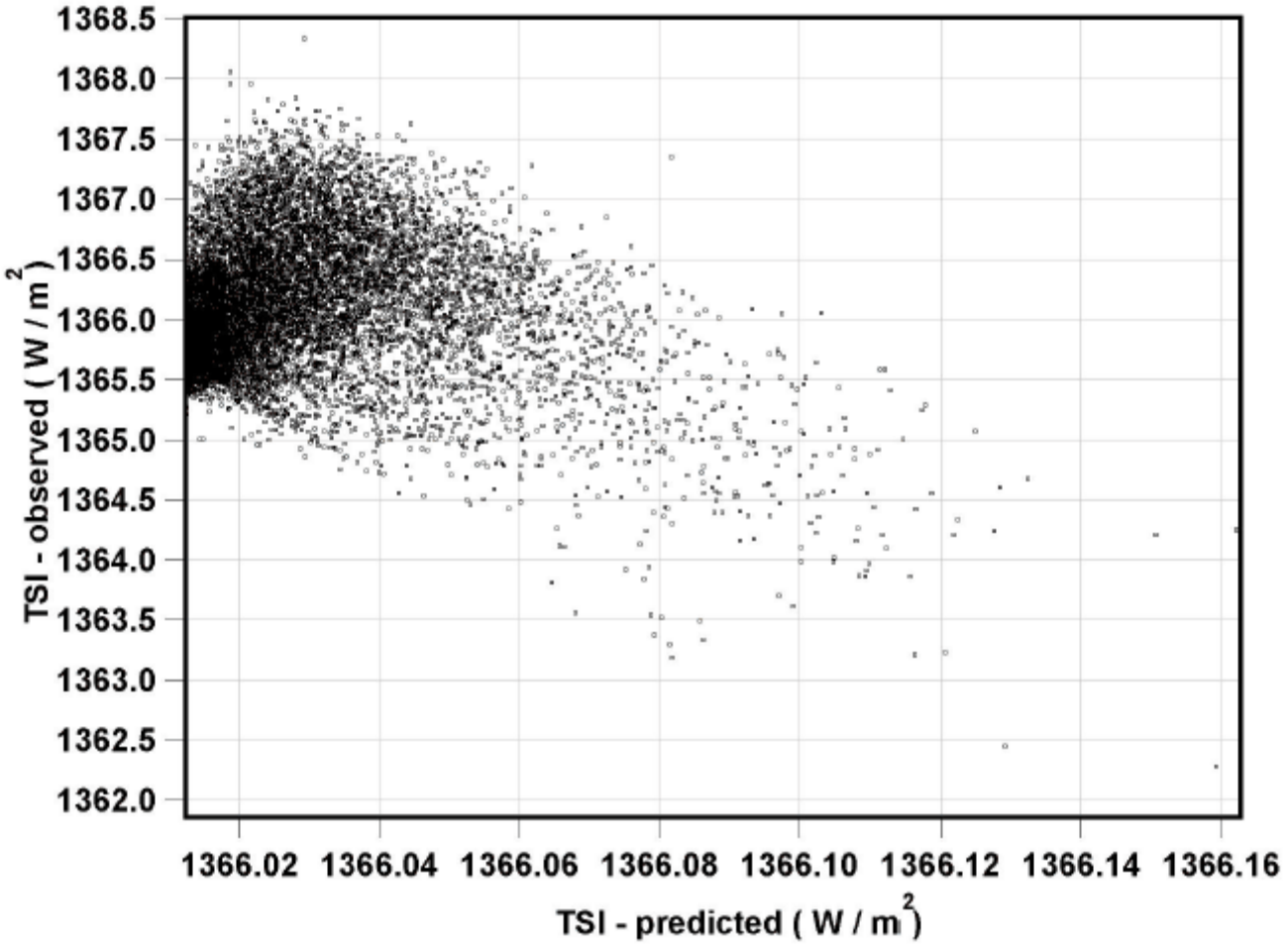


Fig. 7. Common parts of the PMOD and PSI are practically uncorrelated (R_c = 0.0300). Here we use predicted-observed crossplot as we will do below for more general than trivial linear regression model.

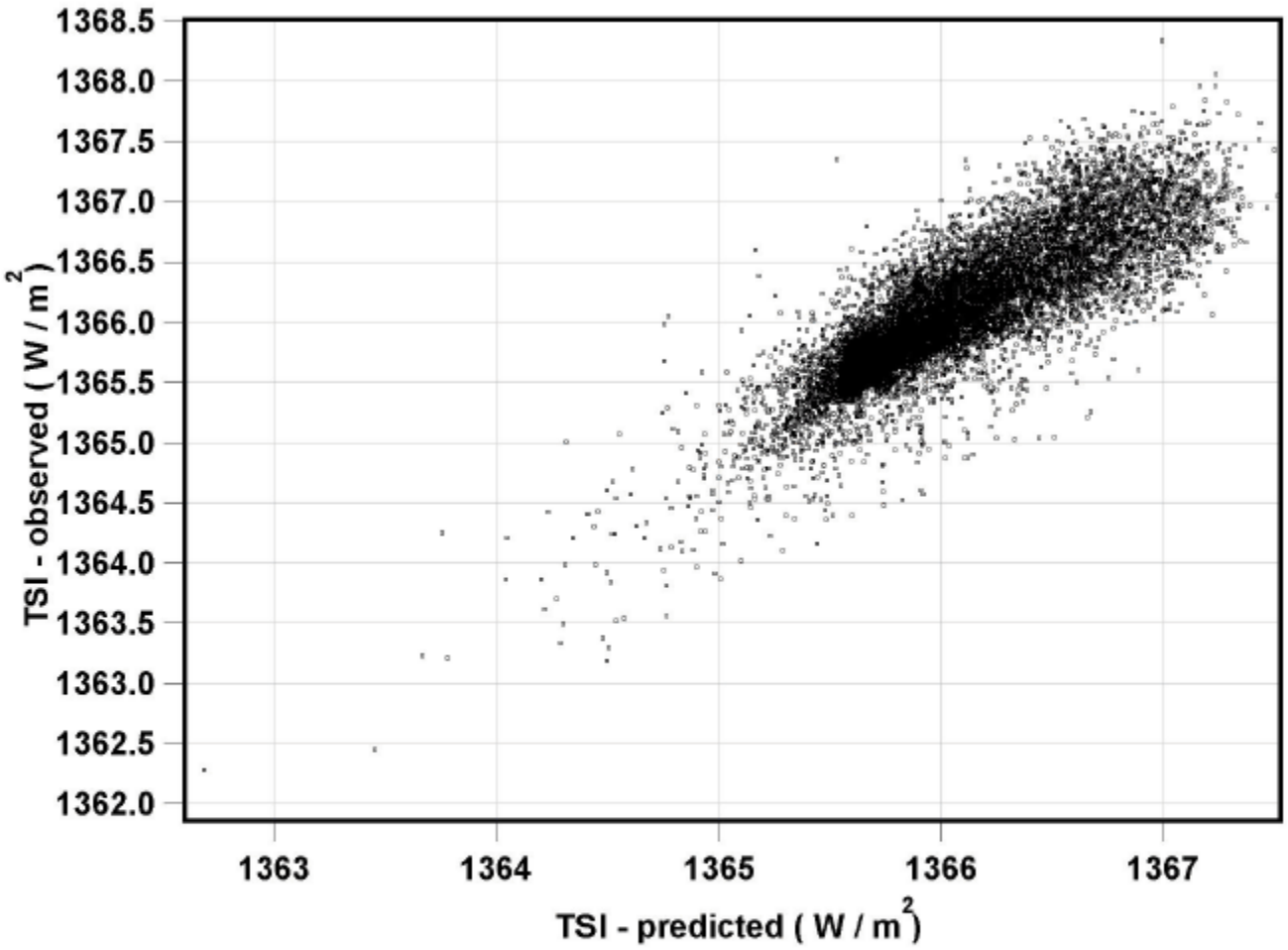


Fig. 9. The observations and simple model with smoothed component is much more strongly correlated (R_c = 0.8597).

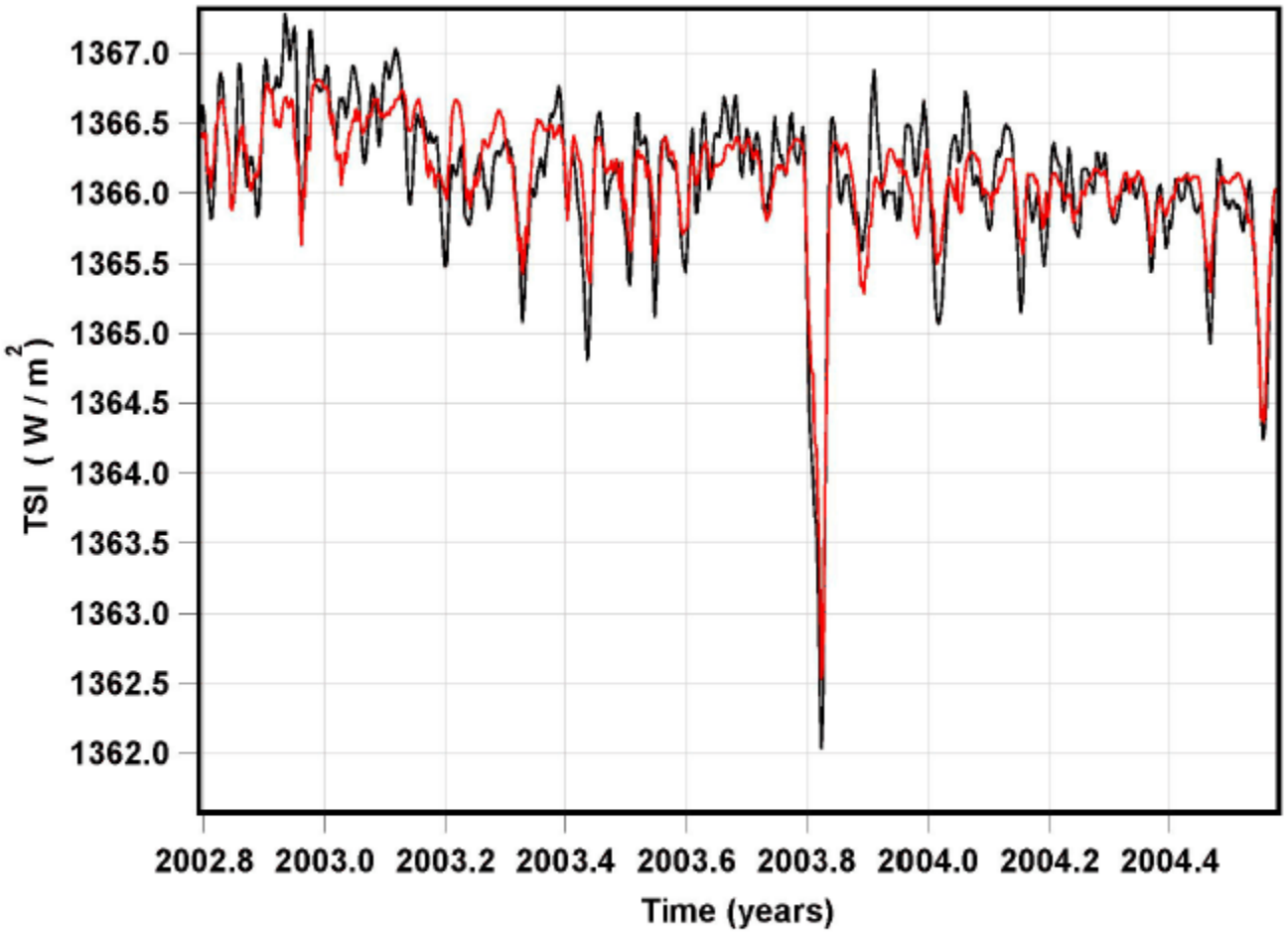


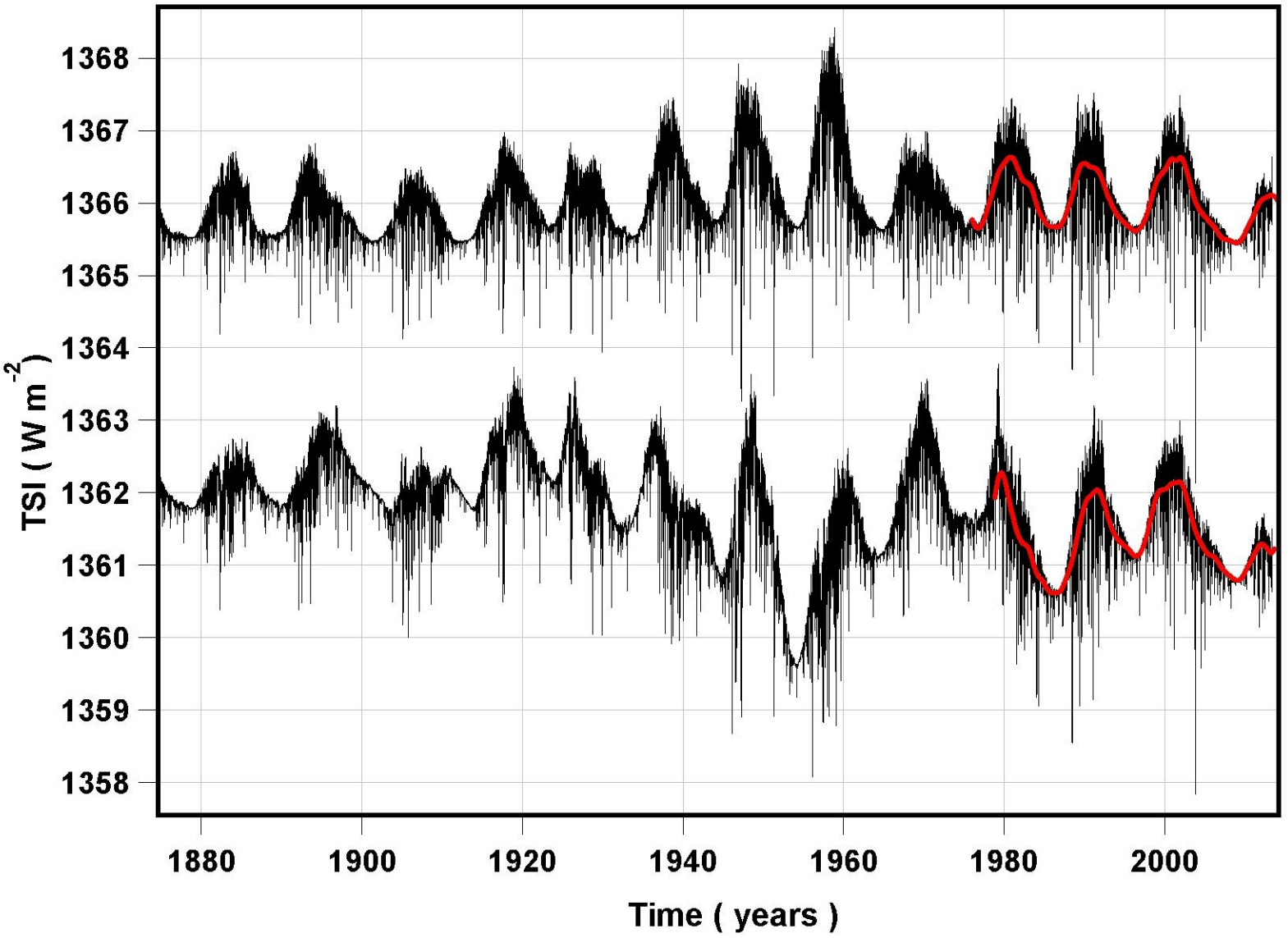
Fig. 10. Reconstruction of the TSI using the HF part of PSI combined with LF part of PMOD. Reconstruction is plotted in red, target in black.

N	Type	Width	1/Offset	R_c
1	E	766.229110	-	0.85973057
2	E_t^+	399.116082	27.103323	0.87599719
3	E^-	2413.855149	1811.476298	0.88710035
4	E	10.083440	10.148801	0.89328020
5	E^-	137.021917	102.081918	0.89713987
6	E^+	3509.347248	12.475225	0.90071914
7	E^+	2474.591733	20.816371	0.90294868
8	E^-	11.057883	10.679024	0.90478582
9	E_t^-	12.699491	11.198220	0.90733729
10	E_t^+	133.649130	188.570202	0.90864964
11	E_t^+	189.738179	198.084112	0.91081665
12	E_t^-	901.197452	28.196168	0.91161825
13	E_t^+	5170.005637	140.675553	0.91222860
14	E_t^+	2544.129259	31.414278	0.91284601
15	E_t^-	33.610573	9.976299	0.91336121

Table 8. Modeling PMOD using PSI data. First 15 components from the greedy search for regression components. Parameters W and O are selected without restrictions.

N	Type	Width	1/Offset	Correlation
1	E_t^+	5170.005661	4419.832453	0.78193389
2	E_t^+	2519.302633	1630.468830	0.83406728
3	E^+	1503.913332	289.744282	0.85372950
4	E^-	3406.542205	148.810590	0.87693631
5	E	362.381918	27.341738	0.88562065
6	E_t^+	430.606068	2183.735031	0.89144597
7	E^-	2340.484301	300.893810	0.89771429
8	E^-	165.079222	93.264999	0.90193772
9	E	9.637961	10.600217	0.90548052
10	E^+	2570.699109	27.380182	0.90766399
11	E_t^+	15.521919	34.876082	0.90919779
12	E^-	1931.046907	289.584617	0.91083821
13	E_t^+	124.463532	112.081094	0.91196667
14	E_t^+	95.268221	105.427923	0.91497974
15	E_t^+	153.399257	109.674353	0.91650578

Table 9. Modeling ACRIM using PSI data. First 15 components from the greedy search for regression components. Parameters W and O are selected without restrictions.


1368
1367
1366
1365
1364
1363
1362
1361
1360
1359
1358
TSI (W m-2)
1880
1900
1920
1940
1960
1980
2000
Time (years)

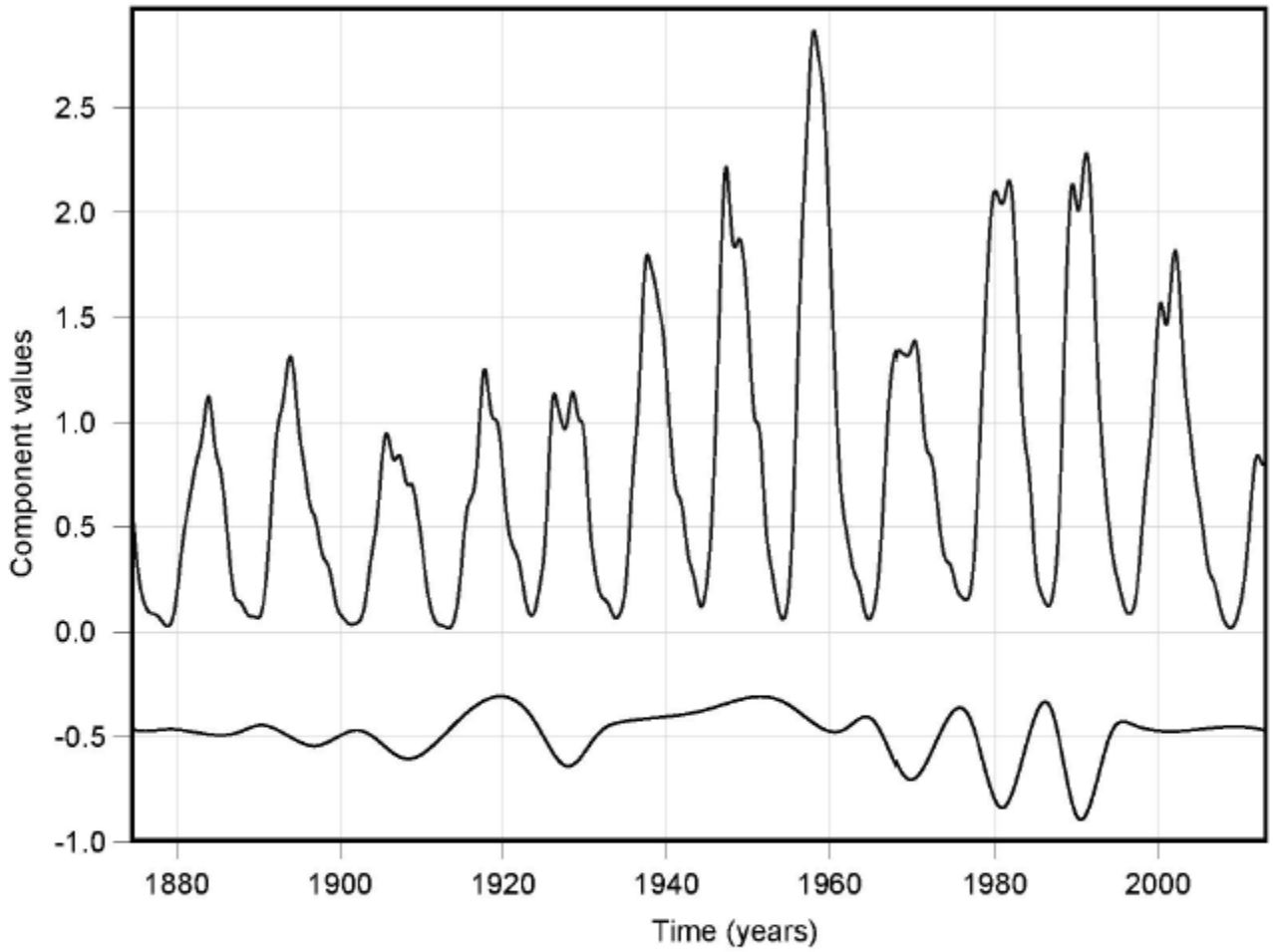


Fig. 14. The first (upper) and third (lower) components of the full scale PSI to PMOD model.

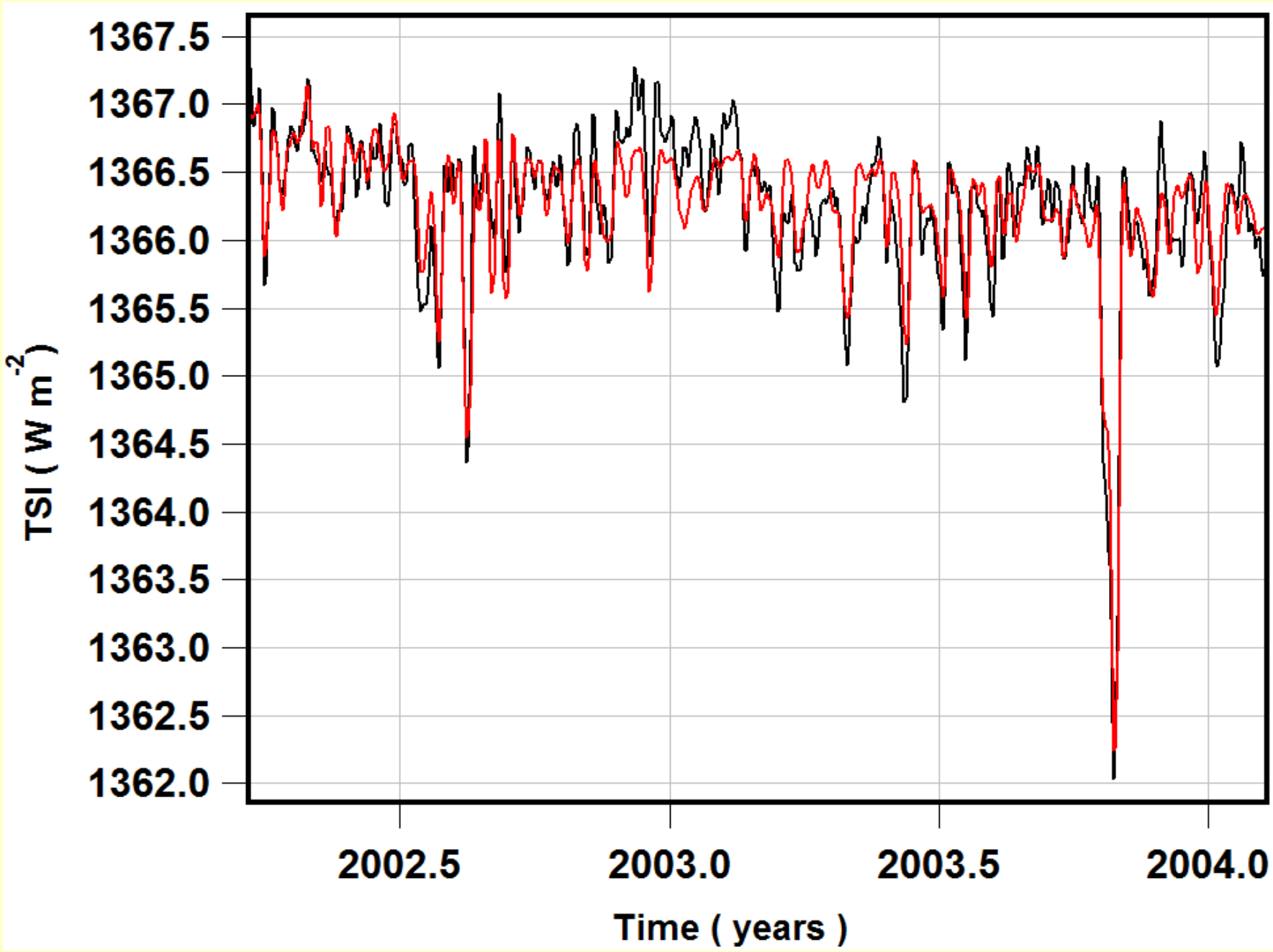
Cross-prediction and sieving

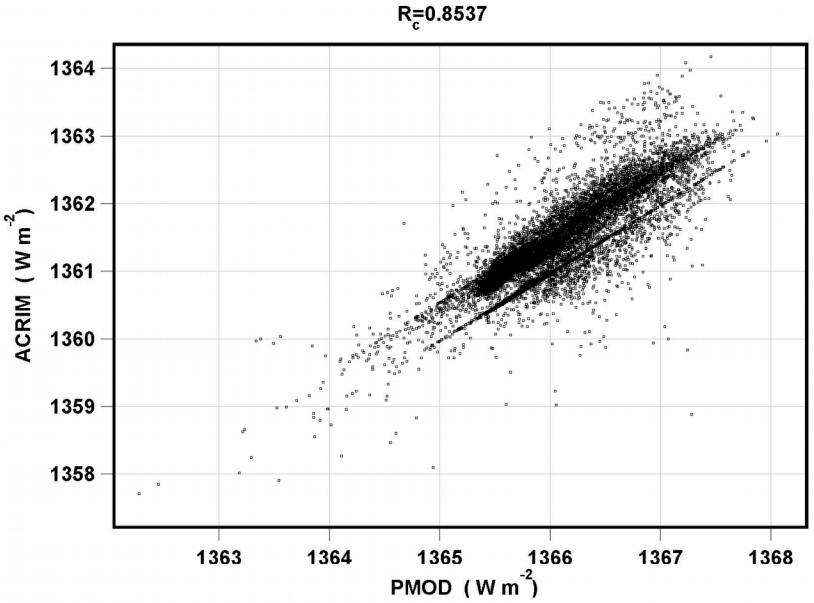
$$R_c = \max_{W,O,M} \min(R_c^{I \to II}(W, O, M), R_c^{II \to I}(W, O, M))$$

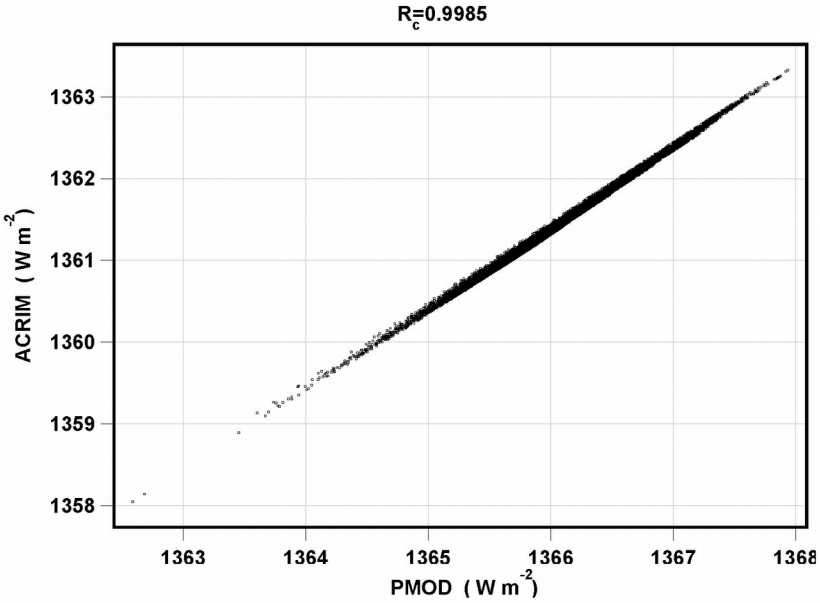
W<2000
1/O<500
Check for colinearity

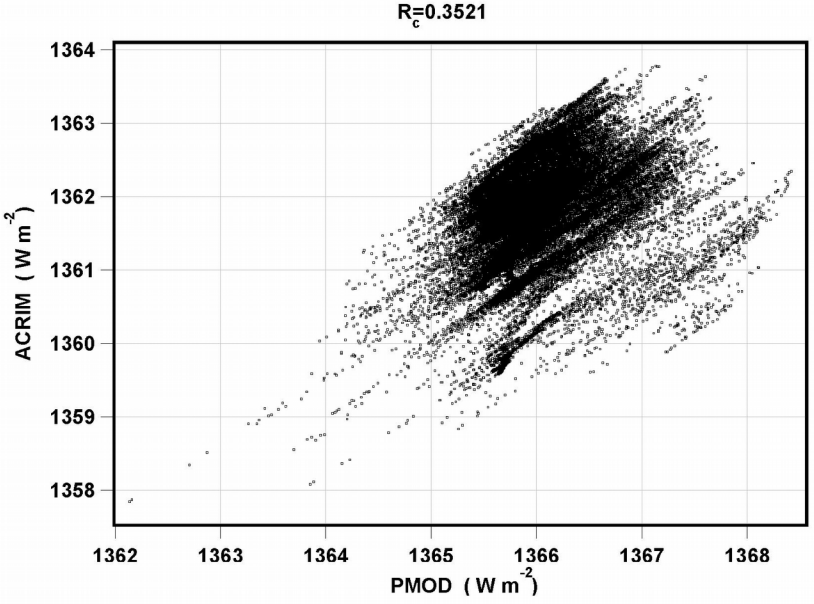
Component	Type	Width	1/Offset	Correlation
1	E	766.203360	-	0.85971218
2	E	368.344694	27.205664	0.87183687
3	E	11.076777	10.507722	0.87798356
4	E	510.918696	-	0.87798440
5	E_t^-	126.141442	85.206093	0.88078618
6	E^-	137.407018	9.624734	0.88213771
7	E_t^-	8.636770	8.672939	0.88481412
8	E^+	356.511603	61.922806	0.88584926
9	E	194.211239	8.970496	0.88652112
10	E^+	124.335750	112.065571	0.88693209
11	E_t^+	145.786806	194.401278	0.88695375
12	E^+	145.491923	169.169762	0.88977830
13	E^+	815.678995	82.630138	0.89115533
14	E_t^+	99.363542	89.764059	0.89158876
15	E	173.673683	77.786024	0.89236231

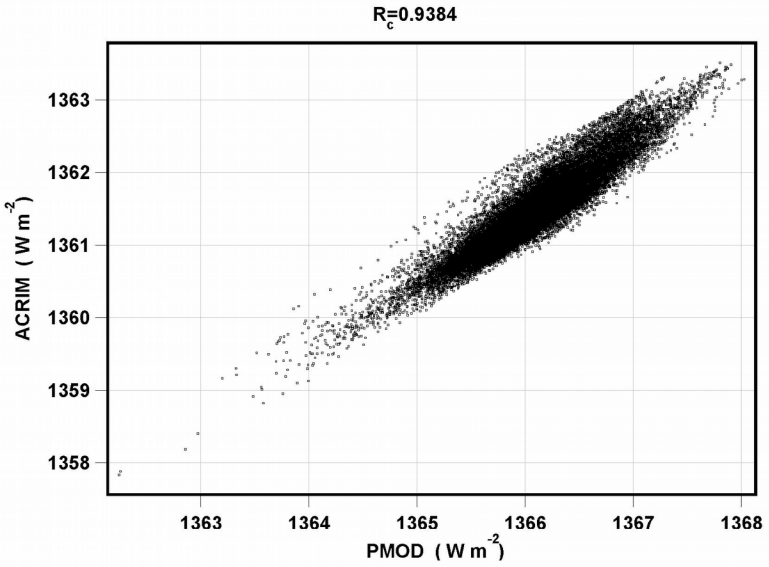
Table 10. Modeling PMOD data using PSI as a proxy. First 15 components of the regression model where all kind of components were allowed.


1367.5
1367.0
1366.5
1366.0
1365.5
1365.0
1364.5
1364.0
1363.5
1363.0
1362.5
1362.0
TSI (W m-2)
2002.5
2003.0
2003.5
2004.0
Time (years)


R_c=0.8537
ACRIM (W m^-2)
PMOD (W m^-2)
1358
1359
1360
1361
1362
1363
1364
1363
1364
1365
1366
1367
1368


R_c=0.9985
ACRIM (W m^-2)
PMOD (W m^-2)
1358
1359
1360
1361
1362
1363
1363
1364
1365
1366
1367
1368


R_c=0.3521
ACRIM (W m^-2)
PMOD (W m^-2)
1358
1359
1360
1361
1362
1363
1364
1362
1363
1364
1365
1366
1367
1368


R_c=0.9384
ACRIM (W m^-2)
PMOD (W m^-2)
1358
1359
1360
1361
1362
1363
1363
1364
1365
1366
1367
1368

Summary

- The correlations between time series depend on frequency band involved.
- The models based on smoothed, enveloped etc components can be used for prediction, interpolation and stitching of different fragments.
- Current state of affairs with TSI measurement and composite building is very complicated.
- Probably the best data product which can be given to climatologists is nearly primitive model based only on small number of components. It will with high probability correlate with true TSI at the level of R_c=0.85 or so.